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Thermal, mechanical and magnetic properties of functionalized magnetite/vinyl ester nanocomposites†

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Magnetite (Fe₃O₄) nanoparticles grafted with thiol groups through silanization of (3-mercaptopropyl) trimethoxy-silane (Fe₃O₄-SH) were used for preparing vinyl ester resin (VER) nanocomposites with different Fe₃O₄ nanoparticle loading levels. The calculated thiol group graft percentage of only ~2.25% did show a significant effect on the physicochemical properties of VER nanosuspensions and nanocomposites. The exothermal curing peak temperature was shifted from 80 °C for pure VER to 75 °C for liquid VER with 10 wt% Fe₃O₄-SH. The tensile strength (72.6 MPa) of 5 wt% Fe₃O₄-SH reinforced nanocomposites was increased by 26.3% as compared with that (57.5 MPa) of pure VER composites. However, the tensile strength (62.7 MPa) of 5 wt% Fe₃O₄ was just increased by 9.0%. The polymer matrix and surface coating were observed to have negligible effects on the magnetic properties of nanoparticles, exhibiting superparamagnetic behaviors.

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1. Introduction

Vinyl ester resin (VER), a well-known thermosetting polymer obtained from the reaction between α,β -unsaturated acids and epoxy resins,^{1,2} the performance of VER lies between that of unsaturated polyester and epoxy resins,³ has been widely used in marine technology, chemical tanks and as a matrix for composite fabrication due to its high corrosion and water resistance,⁴⁻⁶ and VER has relatively high moduli, strength, and glass transition temperature while maintaining low weight and cost.^{7,8}

Magnetic nanoparticles with a size close to the single-domain are of tremendous interest in different fields of chemistry and physics due to their unique magnetic properties such as high coercivity and chemical catalytic properties inherent with their small size and high specific surface area.⁹⁻¹¹ The magnetic nanoparticles have great potential to be applied in a wide range of disciplines, including magnetic fluids,^{12,13} catalysis,¹⁴ biotechnology and biomedicine,¹⁵ magnetic resonance imaging,¹⁶ data

storage,¹⁷⁻¹⁹ magnetic sensing,²⁰⁻²² electromagnetic interference shielding,^{23,24} and environmental remediation.²⁵ The magnetite (Fe₃O₄) is oxidation state and it can't be oxidized further, however Fe, Co and Ni are easily oxidized during its usage. Compared with low magnetization of γ -Fe₂O₃ around 35 emu g⁻¹, Fe₃O₄ has a relatively larger magnetization (around 60 emu g⁻¹) among all natural minerals on earth.^{26,27} Fe₃O₄ is a mixed iron oxide with a cubic inverse spinel structure, AB₂O₄,²⁸ where the A site is occupied by Fe³⁺ ion, and octahedral B sites are occupied by an equal number of randomly distributed 2⁺ and 3⁺ Fe ions.²⁹ Fe₃O₄ is a half-metallic ferromagnetic material, in which the density of state at the Fermi level $N(E_F)$ is completely polarized and the conductivity is determined by the metallic electron spin charge carriers because of the coexistence of metallic electron spin and insulating electron spin.^{28,30} Fe₃O₄ with a lot of unique catalytic, magnetic, and electrical properties^{28,31,32} has been widely applied in many fields such as biomedicine, information storage, color imaging, cell separation, environment remediation,³³ and magnetic structural nanocomposites.³⁴ Incorporating the Fe₃O₄ nanoparticles into polymer matrix can broaden their deployments in electronic, biomedical, and magnetic fields.³⁵⁻³⁸

The composite materials containing magnetic nanoparticles not only have the intrinsic properties of the magnetic nanoparticles but also possess properties of the polymer. VER combined with nano-Fe₃O₄ is a kind of polymer nanocomposites possessing the performance of VER and the properties of Fe₃O₄ (such as magnetism). Different reagents have been used to modify Fe₃O₄ for usages in many fields.³⁹⁻⁴¹ Meanwhile, different methods and materials have been used to modify VER to obtain good performances with many unique

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properties. For example, Li *et al.*⁴² used multifunctional polyhedral oligomeric silsesquioxane to improve the thermal stabilities, flexural strength, modulus and hardness of VER. Thostenson *et al.*⁴³ have reported a technique to disperse the nanotubes in a vinyl ester monomer synthesized from an epoxy precursor for a potential usage as sensors in traditional fiber composites. Guo *et al.*⁴⁴ functionalized $\gamma\text{-Fe}_2\text{O}_3$ nanoparticles with bi-functional coupling agent to increase thermal stability and mechanical properties. J. Karger-Kocsis *et al.*^{45–49} have made a series of efforts dedicated to the modification of VER. They used a novolac-based polyisocyanate (NPI) to modify the VER, the polyisocyanate-containing systems were termed VEUH, finding that adding NPI improved markedly the T_g values of the resins. VEUH was then toughened by adding various vinyl-functionalized branched polyethers and a set of six-arm star polymers. It was established that VER hybridized with other resins can be improved toughness with different toughening methods. They also found that hybridization of acrylated epoxidized soybean oil with vinyl ester is a promising strategy to develop hybrid resins with tailored thermal and mechanical properties, which are suited for engineering applications. The researches of vinyl ester resins modified with organophilic synthetic layered silicates and multiwall carbon nanotube have also performed. The results found that the fracture toughness and energy of composites were markedly improved with increasing organophilic synthetic layered silicates amount, and the electrical conductivity has improved much larger than on the fracture mechanical performance of composites modified with multiwall carbon nanotube. However, the Fe_3O_4 nanoparticles grafted with (mercaptopropyl) trimethoxy-silane (thiol group) to prepare the VER nanocomposites and their effects on the properties of VER nanocomposites have not been reported. Thiol-ene reactions, in both radical and base/nucleophilic forms, are able to change surface properties simply by light exposure.⁵⁰ For example, Goldmann *et al.* reported the functionalization of cross-linked poly(divinylbenzene) microspheres using thiol-ene chemistry. It is really desirable that VER bearing vinyl moieties could be modified by thiol-ene reaction.⁵¹ Thiol-ene reaction could be exploited to build-in the magnetite nanoparticles in the VER network.

In this work, the Fe_3O_4 nanoparticles with surface grafted with thiol groups by using (3-mercaptopropyl) trimethoxy-silane coupling agent ($\text{Fe}_3\text{O}_4\text{-SH}$) have been used to prepare VER nanocomposites to increase the mechanical properties at the same time to introduce magnetization. The surface functional groups of $\text{Fe}_3\text{O}_4\text{-SH}$ were analyzed by Fourier transform infrared (FT-IR) spectroscopy. The grafting ratio of $\text{Fe}_3\text{O}_4\text{-SH}$ and the thermal stability of the cured VER nanocomposites were studied by thermogravimetric analysis (TGA). The crystalline information was studied by X-ray diffraction (XRD). The Brunauer-Emmett-Teller (BET) was measured on the surface areas and pore-size distributions to verify further the introduction of thiol group. The mechanical properties were analyzed by unidirectional tensile testing and dynamic mechanical analyses (DMA). The morphology of the fracture surfaces was characterized with a field emission scanning electron microscope (SEM).

2. Experimental

2.1 Materials

The vinyl ester resin (VER, Derakane momentum 411-350, Dow Chemical Company) was a mixture of 55 wt% vinyl ester with an average molecule weight of 970 g mol^{-1} and 45 wt% styrene monomers. Styrene with only one unsaturated carbon-carbon double bond will provide linear chain extension. Vinyl ester monomers with two reactive vinyl end groups will enable the cross-linking for network formation. The liquid resin has a density of 1.045 g cm^{-3} and a viscosity of 350 mPa s at room temperature. Methyl ethyl ketone peroxide (MEKP) (curing catalyst or initiator, organic peroxide, liquid) was purchased from Miller-Stephenson Chemical Company. The Fe_3O_4 nanoparticles were obtained from Nanjing Emperor Nano Material Co., Ltd., China. The grafting agent (3-mercaptopropyl) trimethoxy-silane and 2-propanol solvent were purchased from Fisher Scientific Company LLC (all chemical structures shown in ESI S1†).

2.2 Preparation of thiol-based Fe_3O_4 nanoparticles

The preparation of Fe_3O_4 containing thiol groups ($\text{Fe}_3\text{O}_4\text{-SH}$) is briefly described as follows. First, 7 g (3-mercaptopropyl) trimethoxy-silane (thiol group), 80 mL 2-propanol and 0.7 mL deionized water were added into a three-necked flask provided with a mechanical stirrer reflux condensing tube and temperature control system. The mixture was stirred at room temperature for 20 min. Second, 10 g Fe_3O_4 and 120 mL 2-propanol were added into the above mixture, the temperature was increased and maintained at $60\text{ }^\circ\text{C}$ for 5 h with mechanical stirring. Finally, the mixture was filtered, washed several times with 2-propanol, and dried in a vacuum oven at $70\text{ }^\circ\text{C}$ overnight. (The reaction sketch is shown in ESI S2.†)

2.3 Preparation of cured pure VER and its nanocomposites

The as-received or functionalized Fe_3O_4 nanoparticles were dispersed in 35 mL resin on a specific weight percentage basis (3.0, 5.0 and 10.0 wt%). The mixture was mechanically stirred at room temperature for dispersion and then the dispersion was carried out in an ice-water ultrasonic bath for about 1 h. When the temperature of the above particle suspension was increased to room temperature, 2.0 wt% catalyst (MEKP) was added to the suspension and mechanically stirred for 2 min. The solution was poured into silicone rubber molds and cured isothermally at $40\text{ }^\circ\text{C}$ for 4 h. Then the temperature was increased and maintained at $100\text{ }^\circ\text{C}$ for 1 h to accomplish the post curing process. Finally, the mixtures were cooled down naturally to room temperature.

2.4 Characterizations

The functional groups of (3-mercaptopropyl) trimethoxy-silane, as-received and functionalized Fe_3O_4 nanoparticles were analyzed by Fourier transform infrared spectroscopy (FT-IR, a Bruker Inc. Vector 22 coupled with an ATR accessory) in the range of $500\text{--}4000\text{ cm}^{-1}$ with a resolution of 4 cm^{-1} . The

grafting ratio was studied in a thermogravimetric analysis (TGA, TA Instruments, Q-500) with a heating rate of $10\text{ }^{\circ}\text{C min}^{-1}$ under an air and nitrogen flow rate of 60 mL min^{-1} from 30 to $800\text{ }^{\circ}\text{C}$.

The powder X-ray diffraction analysis of the samples was carried out with a Bruker AXS D8 Discover diffractometer with general area detector diffraction system operating with a Cu-K α radiation source filtered with a graphite mono-chromator ($\lambda = 0.1541\text{ nm}$). The specific Brunauer–Emmett–Teller (BET) surface areas and pore-size distributions were measured on a Quantachrome Nova 2200 e by nitrogen adsorption at 77.4 K. Prior to each measurement, the samples were degassed at $300\text{ }^{\circ}\text{C}$ for 24 h under high vacuum ($<0.01\text{ mbar}$). The mesopore-size distribution was calculated by the Barrett–Joyner–Halenda (BJH) method using desorption isotherms.⁵²

Differential scanning calorimeter (DSC, TA Instruments Q2000) measurements were implemented under a nitrogen flow rate of approximately 20 mL min^{-1} at a heating rate of $5\text{ }^{\circ}\text{C min}^{-1}$ from 40 to $200\text{ }^{\circ}\text{C}$. Dynamic rheological measurements were performed isothermally by using environmental test chamber aluminum parallel-plate geometry (25 mm in diameter). For the isothermal test, the shear storage and loss moduli were obtained by operating the measurements isothermally at $40\text{ }^{\circ}\text{C}$ with a sweeping time range between 0 and 300 s at a low strain (1%) in a rheometer (AR 2000 ex, TA Instrumental Company). The thermal stability of the cured VER nanocomposites with different Fe $_3$ O $_4$ loadings and functional groups was studied with thermogravimetric analysis (TGA, TA instruments TGA Q-500). TGA was conducted on the cured pure VER, VER/Fe $_3$ O $_4$ and VER/Fe $_3$ O $_4$ -SH nanocomposites from 30 to $600\text{ }^{\circ}\text{C}$ with an air flow rate of 60 mL min^{-1} and a heating rate of $10\text{ }^{\circ}\text{C min}^{-1}$. Dynamic mechanical analyses (DMA) measurements were carried out in the torsion rectangular mode using an AR 2000 ex (TA Instrumental Company) with a strain of 0.05%, a constant frequency of 1 Hz and a heating rate of $2\text{ }^{\circ}\text{C min}^{-1}$ in the temperature range of $30\text{--}200\text{ }^{\circ}\text{C}$. The sample dimensions were $12 \times 3 \times 40\text{ mm}^3$.

The tensile tests were carried out following ASTM (Standard D 412-98a, 2002) in a universal tensile testing machine (ADMET tensile strength testing system). The parameters (displacement and load) were controlled by a digital controller (MTEST Quattro) with Mtest Quattro Materials Testing Software. The samples were prepared as described for the nanocomposites fabrication in the silicone rubber molds, which were designed according to the standard ASTM requirement. A crosshead speed of 1.00 mm min^{-1} was used and the strain (%) was calculated by dividing the crosshead displacement by the original gauge length. After the tensile test, the broken samples were collected and the morphology of the fracture surfaces was characterized with a field emission scanning electron microscope (SEM, Hitachi S-3400 SEM). The surface topography of the as-received and functionalized Fe $_3$ O $_4$ NPs were also tested by SEM. Before testing, the samples were first coated with a thin gold layer for better imaging. The magnetic properties were investigated in a 9 T Physical Properties Measurement System (PPMS) by Quantum Design.

3. Results and discussion

3.1 Functionalization of Fe $_3$ O $_4$ nanoparticles

Fig. 1A shows the FT-IR spectra of (3-mercaptopropyl) trimethoxy-silane (ESI S3 \dagger), as-received Fe $_3$ O $_4$ and Fe $_3$ O $_4$ -SH. The bands at around 1621 and 3423 cm^{-1} are due to the O–H stretching modes and bending vibration of the free or adsorbed water and the hydroxyl groups of the Fe $_3$ O $_4$.⁵³ The bands at 790 and 1190 cm^{-1} are related to the Si–O characteristic peak of thiol-group (ESI S3 \dagger).⁵⁴ In Fig. 1A(a and b), the sharp peak at 650 cm^{-1} is related to the Fe–O bending vibration.⁵⁵ For the Fe $_3$ O $_4$ -SH spectrum, two Si–O characteristic peaks are observed at 990 and 1240 cm^{-1} . For the as-received Fe $_3$ O $_4$, only Fe–O characteristic peak is observed without the Si–O characteristic peaks. These results show the success of the Fe $_3$ O $_4$ surface grafting with thiol groups by (3-mercaptopropyl) trimethoxy-silane.

X-ray diffraction (XRD) characterization was performed on the Fe $_3$ O $_4$ and Fe $_3$ O $_4$ -SH nanoparticles to reveal the crystalline information. Fig. 1B shows the XRD patterns of the Fe $_3$ O $_4$ nanoparticles with and without thiol groups. The position and intensity of the signals are typical for those of magnetite.⁵⁶ However, all the XRD peaks are observed to be slightly moved to the small angle after thiol functional treatment, Fig. 1B, indicating that the lattice constant becomes bigger than that of the as-received Fe $_3$ O $_4$.⁵⁷ It is due to the introduction of atoms in the silane couple agent and the total atomic radius of silane couple agent is larger than the main atoms in Fe $_3$ O $_4$. For this work, XRD indicates the successful introduction of thiol groups.

In order to investigate the porous structure and surface area, the nitrogen adsorption–desorption isothermals of the Fe $_3$ O $_4$ mesoporous spheres with and without thiol treatment and its corresponding pore size distribution curve are shown in ESI S4, \dagger Fig. 1C and Table 1. The isotherm can be classified as a type IV isotherm characteristic for Fe $_3$ O $_4$ and Fe $_3$ O $_4$ -SH.^{58,59} The type IV isotherm is a characteristic of mesoporous solids with pore diameters between 2 and 50 nm.⁶⁰ The corresponding pore size distribution data calculated from the desorption branch of the nitrogen isotherm by the BJH (Barrett–Joyner–Halenda) method shows that the Fe $_3$ O $_4$ -SH exhibit a lower BET surfaces area and smaller pore than the as-received Fe $_3$ O $_4$ (Table 1). For the as-received Fe $_3$ O $_4$ nanoparticles, a pore size distribution peaking at 4.3 nm was observed, and 3.4 nm for the Fe $_3$ O $_4$ -SH was observed. It is believed that the thiol groups grafted onto the opening of pores caused the closing of some pores and resulted in a reduced surface area and smaller pore size.

Fig. 1D shows the TGA curves of the as-received Fe $_3$ O $_4$, Fe $_3$ O $_4$ -SH and (3-mercaptopropyl) trimethoxy-silane (ESI S5 \dagger) in nitrogen. For the as-received Fe $_3$ O $_4$ and Fe $_3$ O $_4$ -SH nanoparticles, a similar initial decomposition temperature around $150\text{ }^{\circ}\text{C}$ is observed due to the loss of moisture. However, different weight loss is observed between the as-received Fe $_3$ O $_4$ and Fe $_3$ O $_4$ -SH from 30 to $800\text{ }^{\circ}\text{C}$. For the as-received Fe $_3$ O $_4$ nanoparticles, a weight loss of 6.8% is observed at $800\text{ }^{\circ}\text{C}$ due to decomposition of the hydroxyl groups on the as-received Fe $_3$ O $_4$ surface. After grafted with (3-mercaptopropyl) trimethoxy-silane, Fe $_3$ O $_4$ has many thiol groups and a weight loss of 8.9% is observed at

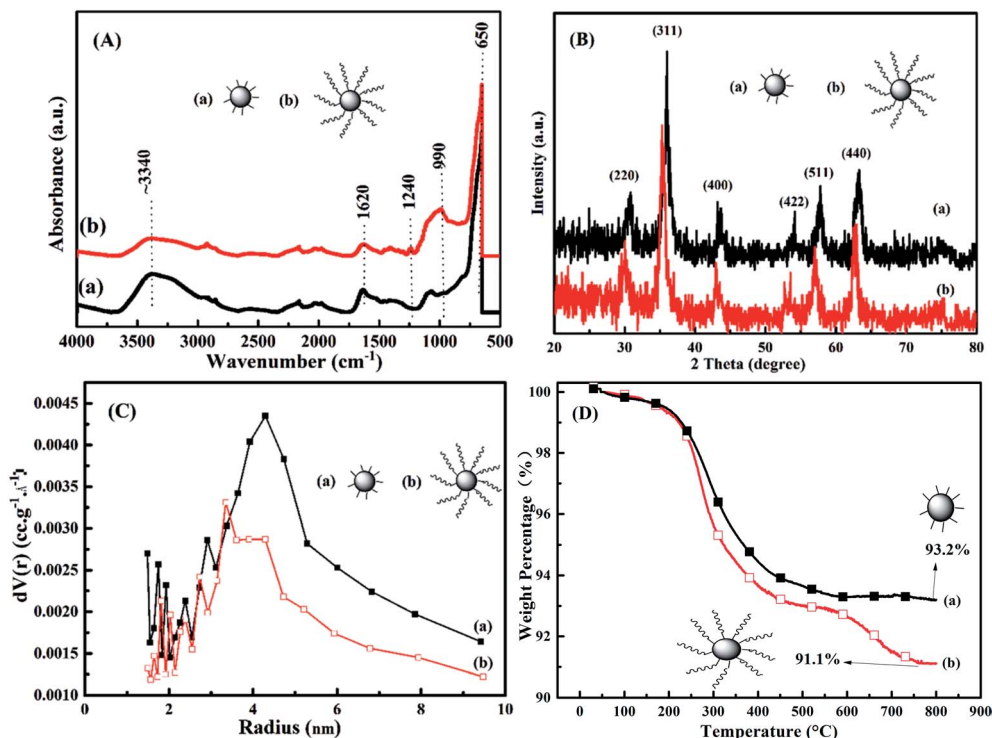


Fig. 1 (A) FT-IR spectra, (B) XRD profiles, (C) pore-size distribution, and (D) TGA profile of (a) as-received Fe_3O_4 and (b) $\text{Fe}_3\text{O}_4\text{-SH}$.

Table 1 Specific surface area and pore size from BET test

Particles	BET surface area ($\text{m}^2 \text{g}^{-1}$)	Average pore size (nm)
As-received Fe_3O_4	110.3	4.3
$\text{Fe}_3\text{O}_4\text{-SH}$	83.0	3.4

800 °C due to decomposition of thiol groups. The grafting ratio can be calculated through eqn (1):⁶¹

$$G = \left(1 - \frac{W_1}{W_0}\right) \times 100\% \quad (1)$$

where G is grafting ratio, W_1 is weight percentage of $\text{Fe}_3\text{O}_4\text{-SH}$ after TGA test and W_0 is the weight percentage of as-received Fe_3O_4 after TGA test, the G is calculated to be around 2.25%.

3.2 Curing process

The isothermal curing behaviors of the VER with Fe_3O_4 and $\text{Fe}_3\text{O}_4\text{-SH}$ nanoparticles were studied using DSC. The DSC thermograms of pure VER, VER with Fe_3O_4 and $\text{Fe}_3\text{O}_4\text{-SH}$ nanoparticles are shown in Fig. 2. The curing for all the samples starts at nearly the same temperatures (~ 40 °C). However, the curing peaks of VER, VER with Fe_3O_4 and $\text{Fe}_3\text{O}_4\text{-SH}$ are different and depend on the loading and functional groups. For the as-received Fe_3O_4 , with increasing the loading of Fe_3O_4 , the shape of curing peak becomes broad and the curing exothermal peak shifts from 80 (VER) to 99 °C (VER with 10.0 wt% Fe_3O_4 nanoparticles). The crosslinking enthalpy (ΔH , J g^{-1}) was also

increased with the loading of Fe_3O_4 . The effect of Fe_3O_4 may like a retardant. The as-received Fe_3O_4 nanoparticles have hydroxyl groups, which hardly react with double bonds of VER or styrene. If there are too many Fe_3O_4 nanoparticles in VER, the cross-linking of the VER monomers would be decreased. ΔH was increased further than that of Fe_3O_4 for the $\text{Fe}_3\text{O}_4\text{-SH}$ and the curing peak becomes sharper and the heat flow is increased significantly, indicating that the curing process could be done in a shorter time and the crosslink of VER had a drastic action due to the thiol group. When the loading of $\text{Fe}_3\text{O}_4\text{-SH}$ is 10.0 wt%, the curing exothermal peak of VER shifts from 80 to

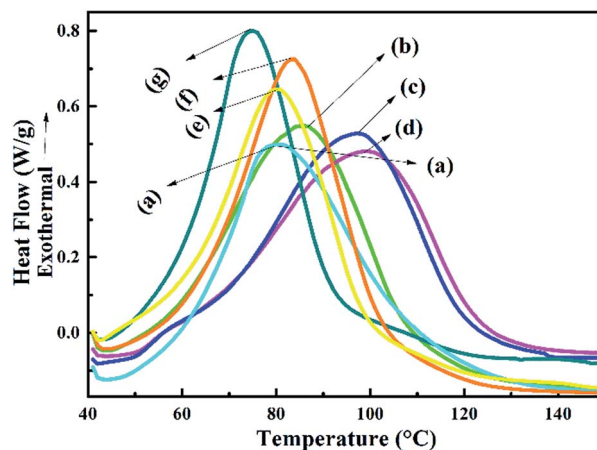


Fig. 2 DSC thermograms of (a) pure VER, liquid VER nanosuspensions with (b) 3.0, (c) 5.0, and (d) 10.0 wt% Fe_3O_4 , (e) 3.0, (f) 5.0, and (g) 10.0 wt% $\text{Fe}_3\text{O}_4\text{-SH}$ nanoparticles.

75 °C due to the existence of thiol group (ESI S6†). The reaction rate of thiol group with styrene is twelve times faster than that of the double bond in VER with styrene.^{62,63} When the Fe₃O₄-SH nanoparticles were dispersed in the VER, the functional group would promote the polymerization process.

3.3 Gelation time for VER with Fe₃O₄ and Fe₃O₄-SH

Gelation time (gel time) is the time interval required for a colloidal solution to become a solid or semisolid jelly or gel. Fig. 3 shows the shear storage modulus (G') and loss modulus (G'') of VER as a function of time at different isothermal curing temperatures. At the very beginning of the curing process ($t = 0$ s), VER is in liquid phase and more energy is dissipated than stored with higher G'' than G' . With proceeding the curing process, both G' and G'' increase and the increment of G' is more rapid than that of G'' , attributed to the network formation of the thermosetting materials, and the sample changes from more liquid like behavior to more solid like behavior.⁶⁴ With further increasing the cross-link density, the value of G' becomes equal to that of G'' , and the corresponding time of the crossing-point of G' and G'' is defined as gel time. After reaching the gel point, the sample turns to more elasticity and more energy is stored than dissipated with G' higher than G'' .⁶⁵ The gel time (in molecular terms, it refers to the point, at which an infinite network is formed) at different curing temperatures is summarized in Table 2.

It is worth noting that the loading of Fe₃O₄ has an influence on the gel time. The gel time becomes longer with increasing the load of the as-received Fe₃O₄. However, after thiol group grafted on the Fe₃O₄ surface, the gel time becomes shorter with increasing the load of Fe₃O₄-SH compared with that of pure Fe₃O₄. If there are Fe₃O₄ particles in VER, the curing process would be prevented. With increasing the load of Fe₃O₄, the gel time becomes longer. The existed Fe₃O₄-SH particles promoted the curing process of VER. With increasing the load of Fe₃O₄-SH, the gel time becomes shorter.

3.4 Thermal stability of cured VER nanocomposites

The thermal stability of the cured VER and its Fe₃O₄ nanocomposites with and without thiol functional nanoparticles was

Table 2 Gel time and crosslinking enthalpy of liquid VER with different Fe₃O₄ nanoparticle loading levels

Composition	t_g (s)	ΔH (J g ⁻¹)
Pure VER	175	110
3.0 wt% Fe ₃ O ₄ -VER	192	159
5.0 wt% Fe ₃ O ₄ -VER	460	163
10.0 wt% Fe ₃ O ₄ -VER	521	169
3.0 wt% Fe ₃ O ₄ -SH-VER	182	166
5.0 wt% Fe ₃ O ₄ -SH-VER	149	171
10.0 wt% Fe ₃ O ₄ -SH-VER	56	180

examined by non-isothermal thermogravimetry. The TGA and differential thermogravimetric (DTG) data obtained for pure VER and its nanocomposites with and without thiol-nanoparticles in air are presented in Fig. 4. From the TGA data, the thermal stability factors, including the initial decomposition temperature (5.0% weight loss, T_1^*), temperature of 50% weight loss (T_2^*), maximum decomposition rate of the first peak (Φ_{m1}^*), maximum decomposition rate of the second peak (Φ_{m2}^*), the temperature of maximum decomposition rate of the first peak (T_{m1}^*), the temperature of maximum decomposition rate of the second peak (T_{m2}^*), and char yield (C.Y) at 600 °C are summarized in Table 3. The TGA and DTG graphs show that all the samples have two main degradation stages. Both the VER/Fe₃O₄ and VER/Fe₃O₄-SH nanocomposites have a lower decomposition temperature for the first and second stage than that of pure VER. The T_1^* , T_2^* , and T_{m1}^* of all the VER/Fe₃O₄ nanocomposites are almost the same as those of the VER/Fe₃O₄-SH nanocomposites, but a little lower than those of pure VER. It indicates that Fe₃O₄ nanoparticles with and without thiol treatment can promote the degradation of VER composites. This is due to the lower decomposition temperature of hydroxyl group in Fe₃O₄ and Si-C bonds in Fe₃O₄-SH than C-O and C-C bonds.^{66,67} And the further decomposition of the second stage is due to the degradation of benzene rings.⁶⁸ The T_{m2}^* of Fe₃O₄/VER with and without thiol groups was also lower than that of pure VER. However, the T_{m2}^* of the VER/Fe₃O₄-SH nanocomposites was a little higher than that of the VER/Fe₃O₄ nanocomposites. This is due to the fact that VER/Fe₃O₄-SH had a little higher crosslinking density than the VER/Fe₃O₄ nanocomposites.

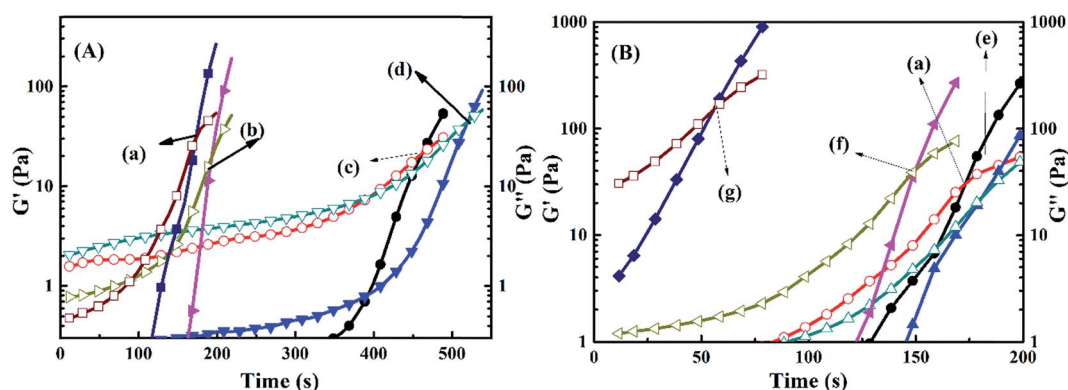


Fig. 3 G' and G'' (open and solid symbols represent G' and G'' , respectively) vs. t of the isothermal curing reaction for (a) pure VER, liquid VER with (b) 3.0, (c) 5.0, and (d) 10.0 wt% Fe₃O₄, (e) 3.0, (f) 5.0 and (g) 10.0 wt% Fe₃O₄-SH nanoparticles.

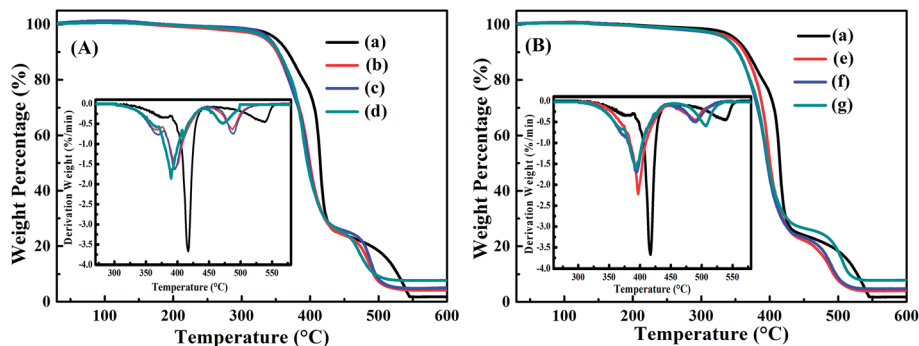


Fig. 4 TGA and DTG curves of (a) pure VER, VER nanocomposites with (b) 3.0, (c) 5.0, and (d) 10.0 wt% Fe_3O_4 , (e) 3.0, (f) 5.0, and (g) 10.0 wt% Fe_3O_4 -SH nanoparticles.

Table 3 TGA data of the VER/ Fe_3O_4 nanocomposites

Composition	Thermal properties						
	T_1^* (°C)	T_2^* (°C)	Φ_{m1}^* (% min ⁻¹)	Φ_{m2}^* (% min ⁻¹)	T_{m1}^* (°C)	T_{m2}^* (°C)	C.Y (600 °C/%)
Pure VER	350	415	3.6	0.4	417	538	1.8
3.0 wt% VER/ Fe_3O_4	334	399	1.6	0.6	396	487	4.2
5.0 wt% VER/ Fe_3O_4	339	398	1.6	0.7	395	488	5.0
10.0 wt% VER/ Fe_3O_4	336	396	1.8	0.5	390	473	7.7
3.0 wt% VER/ Fe_3O_4 -SH	344	400	2.2	0.4	397	490	4.0
5.0 wt% VER/ Fe_3O_4 -SH	336	396	1.7	0.5	395	492	4.8
10.0 wt% VER/ Fe_3O_4 -SH	335	397	1.6	0.6	394	507	7.9

With increasing the loading of Fe_3O_4 nanoparticles, the char yield increased. Higher concentration of Fe_3O_4 increased the char yield of the nanocomposites because the Fe_3O_4 nanoparticles cannot be burned.

3.5 Mechanical properties

Dynamic mechanical analysis (DMA) shows specific information about the storage modulus (G'), loss modulus (G'') and loss factor ($\tan \delta$) within the test temperature range. The G' reflects the elastic modulus or energy storage of the VER nanocomposites while the G'' is related to the viscous behavior or the energy dissipation associated with the motion of polymer chains in the VER nanocomposites.⁶⁸ Fig. 5 shows the G' as

a function of temperature for pure VER and its cured nanocomposites with Fe_3O_4 and Fe_3O_4 -SH nanoparticles. The G' curves show a wave-like shape for the VER/ Fe_3O_4 nanocomposites except the nanocomposites containing 5.0 wt% Fe_3O_4 -SH. That is, the curves have a slight slope except the curve of 5.0 wt% Fe_3O_4 -SH nanocomposites (just one declining curve). The slight slope shown in Fig. 5 is due to the additional curing of the sample.⁶⁴ During the DMA test, with increasing the temperature, the samples enter the glass transition region, and sufficient molecular mobility enables further curing process. With the network formed in the resin, the movement of polymer chains is restrained and the G' value is increased. After the VER is well cured, the samples entering the rubbery region, the G' decreases with increasing the temperature.⁶⁹ It is worth noting

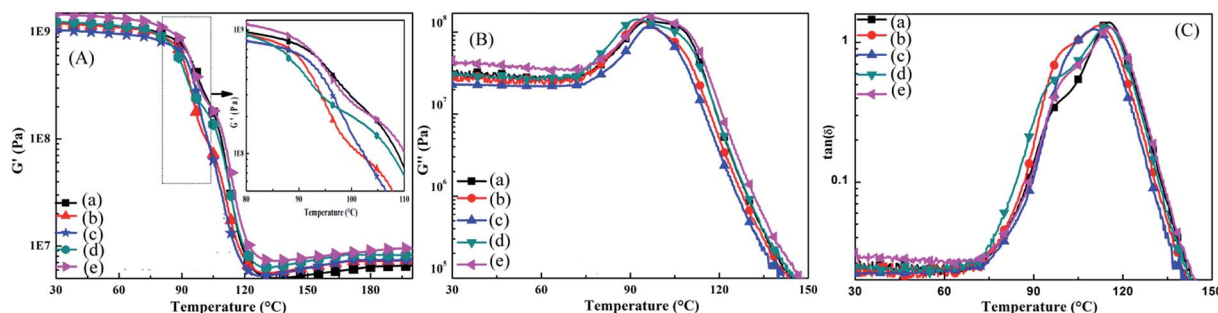


Fig. 5 (A) Storage modulus (G'), (B) loss modulus (G'') and (C) $\tan \delta$ vs. temperature of (a) the cured pure VER, and VER nanocomposites with (b) 5.0 wt% Fe_3O_4 , (c) 5.0 wt% Fe_3O_4 -SH, (d) 10.0 wt% Fe_3O_4 , and (e) 10.0 wt% Fe_3O_4 -SH nanoparticles.

that the 5.0 wt% VER nanocomposites had no additional variation of G' , indicating that the 5.0 wt% Fe_3O_4 -SH nanocomposites were well cured. It also indicates that thiol group has an effect on the curing process of VER. The $\tan \delta$ is the ratio of the G'' to G' and the peak of $\tan \delta$ is often used to determine the glass transition temperature (T_g). The 5.0 wt% Fe_3O_4 -SH nanocomposites exhibit a different curve in the range of 90 to 110 °C from other samples, Fig. 5.

Fig. 6 shows the typical tensile strain–stress curves of the cured VER nanocomposites. The tensile strength of the VER/ Fe_3O_4 nanocomposites is observed to depend on two factors, *i.e.*, the functional group and the nanoparticle loading. For the cured VER nanocomposites containing Fe_3O_4 and Fe_3O_4 -SH nanoparticles, the tensile strength increases with increasing the Fe_3O_4 loading to 5.0 wt% and the tensile strength is decreased significantly with further increasing the Fe_3O_4 up to 10.0 wt%. For the 5.0 wt% Fe_3O_4 nanocomposites with and without thiol functional treatment, the tensile strength of the nanocomposites is around 72.6 and 62.7 MPa, which is increased by 26.3 and 9.0% (crosslink density, $\alpha = 0.97, 0.91$) than that of pure-VER (57.5 MPa, $\alpha = 0.87$), respectively. Compared with pure VER, the tensile strength of the 10.0 wt% Fe_3O_4 nanocomposites is decreased by 8.3% ($\alpha = 0.79$). However, the 10.0 wt% Fe_3O_4 -SH nanocomposites are increased by 5.9% ($\alpha = 0.89$). While the loading of Fe_3O_4 with and without the thiol treatment reached 10.0 wt%, the tensile strength of the nanocomposites was decreased compared with that of 5.0 wt% Fe_3O_4 nanocomposites with and without thiol functional treatment. It is due to the agglomeration of the nanoparticles.³⁴ The agglomerated nanoparticles prevented the crosslinking formation of polymer chains. For the functionalized Fe_3O_4 nanoparticles, the effect of thiol groups is more beneficial to the curing process than the hydroxyl groups on the as-received Fe_3O_4 nanoparticles. The thiol groups involved in the curing of VER, more VER chains were combined together and thus VER became harder to be broken. However, if there were too many Fe_3O_4 -SH, it could make the curing process faster so that the crosslink was not complete, consistent with the gelation time for the VER nanocomposites with Fe_3O_4 and Fe_3O_4 -SH and the DMA results.

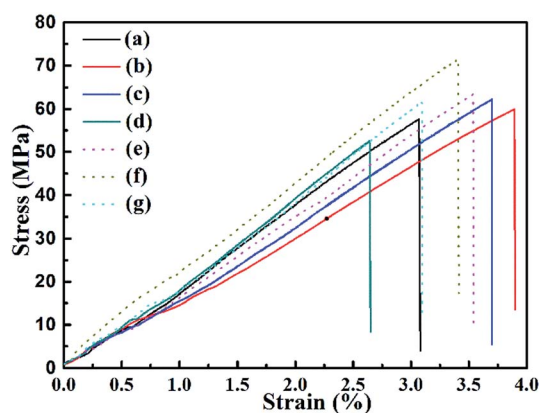


Fig. 6 Stress–strain curve of (a) pure VER, and VER nanocomposites with (b) 3.0, (c) 5.0, (d) 10.0 wt% Fe_3O_4 , (e) 3.0, (f) 5.0, and (g) 10.0 wt% Fe_3O_4 -SH nanoparticles.

From the SEM graph (Fig. 7) of the fracture surface, the cured pure VER shows a smooth and river-like fracture surface, indicating that pure VER is very brittle, typical of thermosetting polymers. The fracture surface becomes much rougher after filled with the as-received and Fe_3O_4 -SH nanoparticles. However, obvious different plastic deformation is observed for the nanocomposites with different particle loadings. The fracture surface of 10.0 wt% Fe_3O_4 -SH nanocomposites is much rougher and much wavier than that of 5.0 wt% Fe_3O_4 -SH. A lot of voids are observed in the fracture surface of 10.0 wt% Fe_3O_4 -SH nanocomposites. This is due to the particles dispersed unevenly in the 10.0 wt% Fe_3O_4 -SH nanocomposites. Some particles were aggregated together and these aggregations were debonded when the nanocomposites were broken, indicating a weak crosslinking in the area of debonding that could lead to a lower tensile strength. For the 10.0 wt% Fe_3O_4 nanocomposites, more aggregations are observed than that of the 10.0 wt% Fe_3O_4 -SH nanocomposites and even the 5.0 wt% as-received Fe_3O_4 nanocomposites were observed to have some aggregations.

3.6 Magnetic properties

Magnetization is a phenomenon that describes the response of magnetic materials to an applied external magnetic field.⁷⁰ The application of a magnetic field could align the magnetic moment of domain in the field direction. The magnetization increases until the magnetic field cannot increase the magnetization of the material further and at this moment the magnetization reaches the saturation magnetization (M_s).^{71,72} When the diameter of magnetic nanoparticles is around 10 nm, the coercive force (H_c) is normally zero, and the nanoparticles are in the super-paramagnetic state. The magnetic properties of a super-paramagnetic system can be described following the Langevin eqn (2):⁷³

$$M = \int_0^{\infty} L\left(\frac{mH}{k_B T}\right) f(m) dm \quad (2)$$

where M is magnetization (emu g^{-1}) in H (Oe), k_B is the Boltzmann constant, m is the magnetic moment, T is the absolute temperature, and $f(m)$ is the distribution function of magnetic moments related to the M_s as described by eqn (3):

$$M_s = \int_0^{\infty} f(m) dm \quad (3)$$

According to eqn (2) and (3), the relationship between M and M_s can be described by eqn (4):

$$\frac{M}{M_s} = \coth x - \frac{1}{x} \quad (4)$$

where, $x = \alpha H$; the parameter α is related to the electron spin magnetic moment m of the individual molecule as described in eqn (5):

$$a = \frac{m}{k_B T} \quad (5)$$

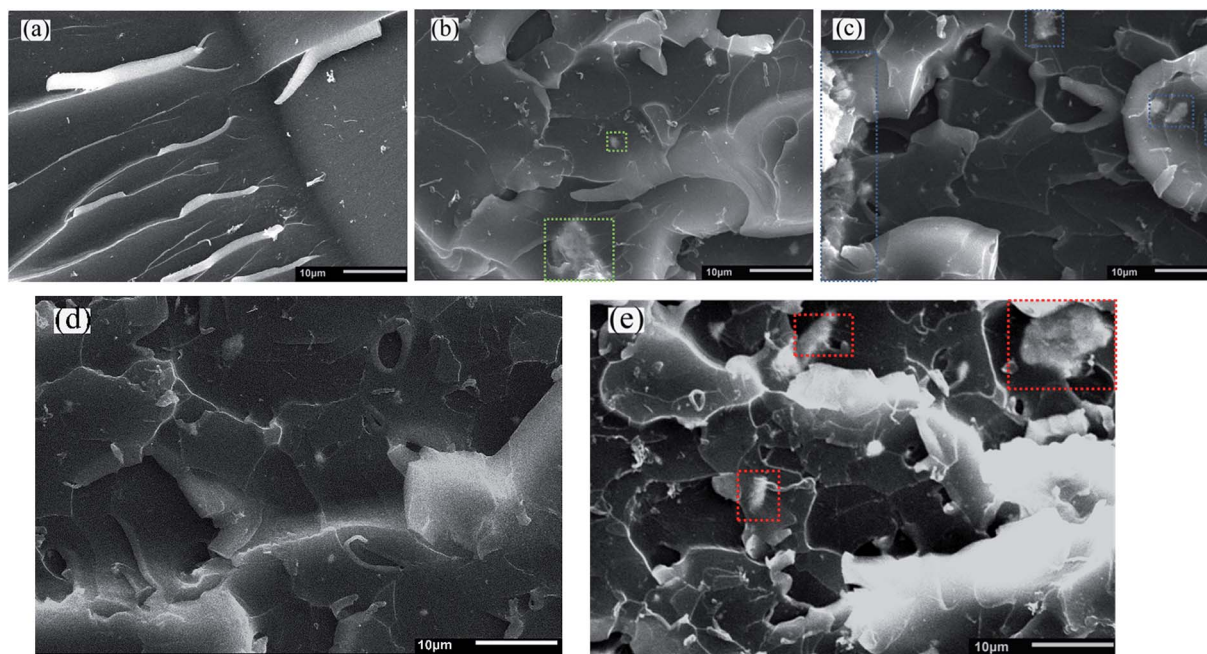


Fig. 7 SEM microstructures of the fracture surface of (a) pure VER and its composites with (b) 5.0, and (c) 10.0 wt% Fe_3O_4 , (d) 5.0, and (e) 10.0 wt% Fe_3O_4 -SH nanoparticles.

Fig. 8 shows the room temperature magnetic hysteresis loops of Fe_3O_4 nanoparticles with and without thiol group, and VER/ Fe_3O_4 nanocomposites with different particle loadings. Pure VER is a non-magnetic material, whereas the VER/ Fe_3O_4 nanocomposites show no hysteresis loops, Fig. 8. The magnetization of all the samples did not reach saturation even at high magnetic field. The M_s is determined by the extrapolated M_s obtained from the intercept of $M-H^{-1}$ at high field.⁷⁴ The calculated M_s of the as-received Fe_3O_4 nanoparticles is 61.9 emu g^{-1} , smaller than that of bulk ($=92\text{--}100 \text{ emu g}^{-1}$).⁷⁵ The calculated M_s of Fe_3O_4 -SH is 60.3 emu g^{-1} , a little smaller than that of the as-received Fe_3O_4 . This is due to the introduction of non-magnetic organic functional groups to Fe_3O_4 . This indicates that the functional group could affect the magnetization of

magnetic nanoparticles. The calculated M_s values of the nanocomposites with and without thiol group nanoparticles at a particle loading of 5.0 and 10.0 wt% are observed to be saturated at a lower field, are 1.8, 3.0, 4.5 and 6.4 emu g^{-1} , respectively. All the samples that are modified with thiol group are observed to have a smaller magnetization than that of the as-received Fe_3O_4 nanoparticles. This indicates that the nanoparticles maintain comparable magnetization in the VER/ Fe_3O_4 nanocomposites to that of the nanoparticles. The nonlinear fitting of magnetization (M) and magnetic field (H) using Poly-math software was applied to obtain the best fit to eqn (4). The parameter α for the as-received Fe_3O_4 and Fe_3O_4 -SH nanoparticles is 3.42×10^{-3} and $3.40 \times 10^{-3} \text{ T}^{-1}$, respectively. For the nanocomposites with and without thiol groups and with

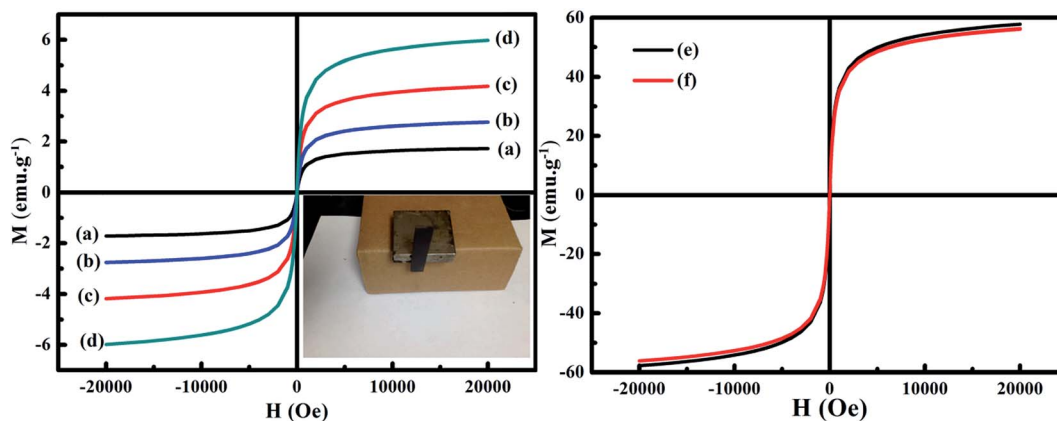


Fig. 8 Room temperature magnetic hysteresis loops of VER nanocomposites with (a) 5.0 wt% Fe_3O_4 -SH, (b) 5.0 wt% as-received Fe_3O_4 , (c) 10.0 wt% Fe_3O_4 -SH, (d) 10.0 wt% as-received Fe_3O_4 , (e) as-received Fe_3O_4 and (f) Fe_3O_4 -SH nanoparticles, inset photo shows the 5.0 wt% VER/ Fe_3O_4 -SH nanocomposites attracted by a magnet.

a particle loading of 5.0 and 10.0 wt%, the parameter α is 3.25×10^{-3} , 3.33×10^{-3} , 3.25×10^{-3} and $3.31 \times 10^{-3} \text{ T}^{-1}$, respectively. The magnetic moment m calculated from eqn (5) for the as-received Fe_3O_4 and $\text{Fe}_3\text{O}_4\text{-SH}$ is 1.48 and 1.47 μ_{B} , respectively. For the nanocomposites with and without thiol group and the particle loading of 5.0 and 10.0 wt%, m is 1.40, 1.40, 1.43 and 1.43 μ_{B} , respectively. At the same loading with different functional group, m is almost the same, indicating that polymer has negligible effect on the magnetic moment of the Fe_3O_4 nanoparticles.²⁸

4. Conclusion

The Fe_3O_4 nanoparticles have been successfully functionalized with thiol group by the coupling agent of (3-mercaptopropyl) trimethoxy-silane. The VER/ Fe_3O_4 nanocomposites with and without thiol groups have been fabricated at different loading levels. SEM indicates that the fracture surface of the nanocomposites became much rougher after filled with $\text{Fe}_3\text{O}_4\text{-SH}$ nanoparticles. Too many particles were dispersed unevenly in the nanocomposites and the agglomerated nanoparticles decreased the tensile strength. The gel time was observed to become longer with increasing the load of the as-received Fe_3O_4 nanoparticles and the gel time became shorter with increasing the load of $\text{Fe}_3\text{O}_4\text{-SH}$ except 3.0 wt% loading. The DMA test indicates that the 5.0 wt% $\text{Fe}_3\text{O}_4\text{-SH}$ nanocomposites were well cured. The tensile test shows that the 5.0 wt% $\text{Fe}_3\text{O}_4\text{-SH}$ nanocomposites have the largest tensile strength. The nanocomposites with and without thiol group appear as superparamagnetic behavior, *i.e.* without a hysteresis loop. The polymer matrix was observed to have negligible effects on the magnetic properties.

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